

Polyphase Representation of a 2-channel F.B.

Suppose $H_0(z) = E_0(z^2) + z^{-1} E_1(z^2)$

If we assume quadrature mirror property,

$$H_1(z) = H_0(-z)$$

$$H_1(z) = E_0(z^2) - z^{-1} E_1(z^2)$$

$$\begin{bmatrix} H_0(z) \\ H_1(z) \end{bmatrix} = \begin{bmatrix} 1 & 1 \\ 1 & -1 \end{bmatrix} \begin{bmatrix} E_0(z^2) \\ z^{-1} E_1(z^2) \end{bmatrix}$$

(Analysis Bank
2 ϕ representation)

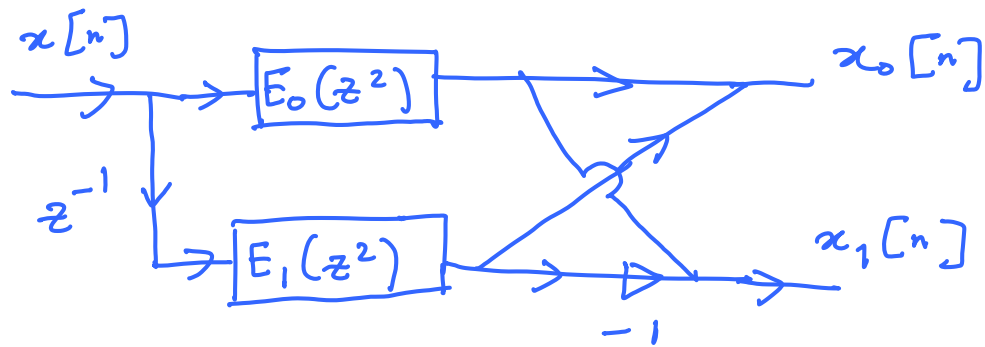
Using alias cancellation conditions,

$$F_0(z) = H_1(-z) \quad ; \quad F_1(z) = -H_0(-z)$$

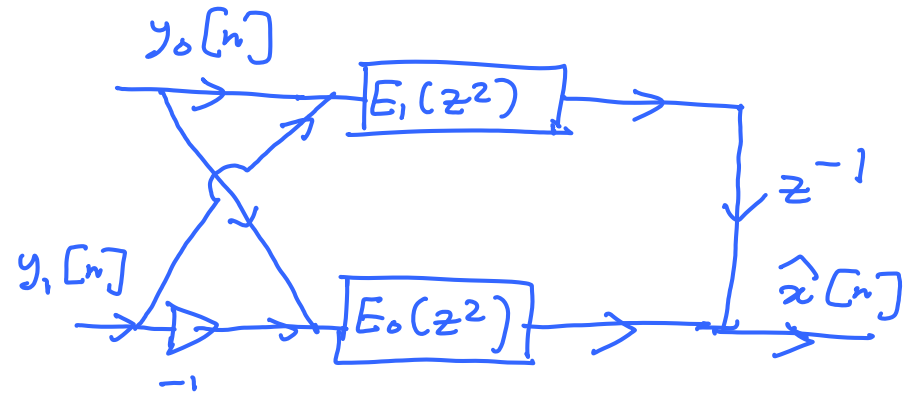
$$\begin{bmatrix} F_0(z) & F_1(z) \end{bmatrix} = \begin{bmatrix} z^{-1} E_1(z^2) & E_0(z^2) \end{bmatrix} \begin{bmatrix} 1 & 1 \\ 1 & -1 \end{bmatrix}$$

Synthesis filters realized
using 2 ϕ representation

Signal Flow Graphs / Representations for poly ϕ realization



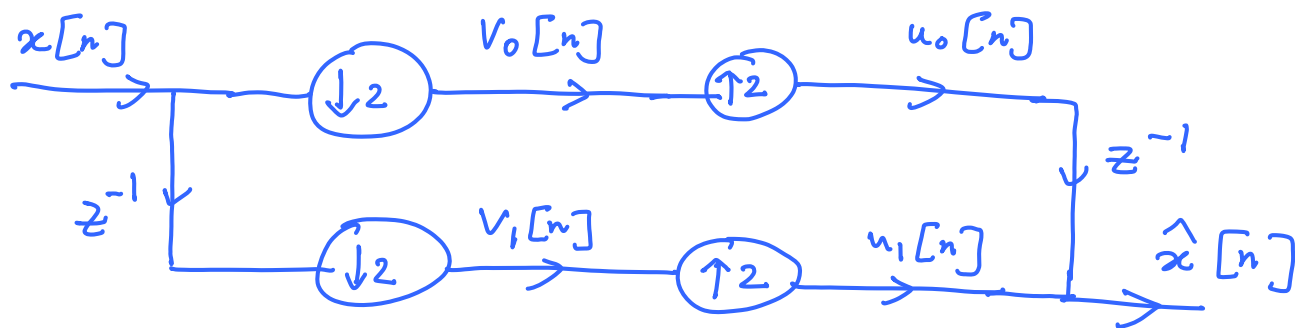
Analysis Bank



Synthesis Bank

Example : 2 - channel perfect reconstruction system

Suppose $H_0(z) = 1$ $H_1(z) = z^{-1}$
 $F_0(z) = z^{-1}$ $F_1(z) = 1$



GOAL: Examine if the system in this example is a P. R. system

Suppose

$$x[n] = \left\{ \begin{array}{cccccccc} 1 & 2 & 3 & 4 & 5 & 6 & 7 & 8 \dots \end{array} \right\}$$

$$v_0[n] = \left\{ \begin{array}{cccc} 1 & 3 & 5 & 7 \dots \end{array} \right\}$$

$$v_1[n] = \left\{ \begin{array}{cccc} x & 2 & 4 & 6 \dots \end{array} \right\}$$

x : dummy

$$u_0[n] = \left\{ \begin{array}{cccccc} 1 & \underline{0} & 3 & \underline{0} & 5 & \underline{0} & 7 \dots \end{array} \right\}$$

$$u_1[n] = \left\{ \begin{array}{cccc} x & \underline{0} & 2 & \underline{0} & 4 & \underline{0} \dots \end{array} \right\}$$

$$u_0[n-1] = \left\{ \begin{array}{cccccc} x & 1 & \underline{0} & 3 & \underline{0} & 5 & \underline{0} & 7 \dots \end{array} \right\}$$

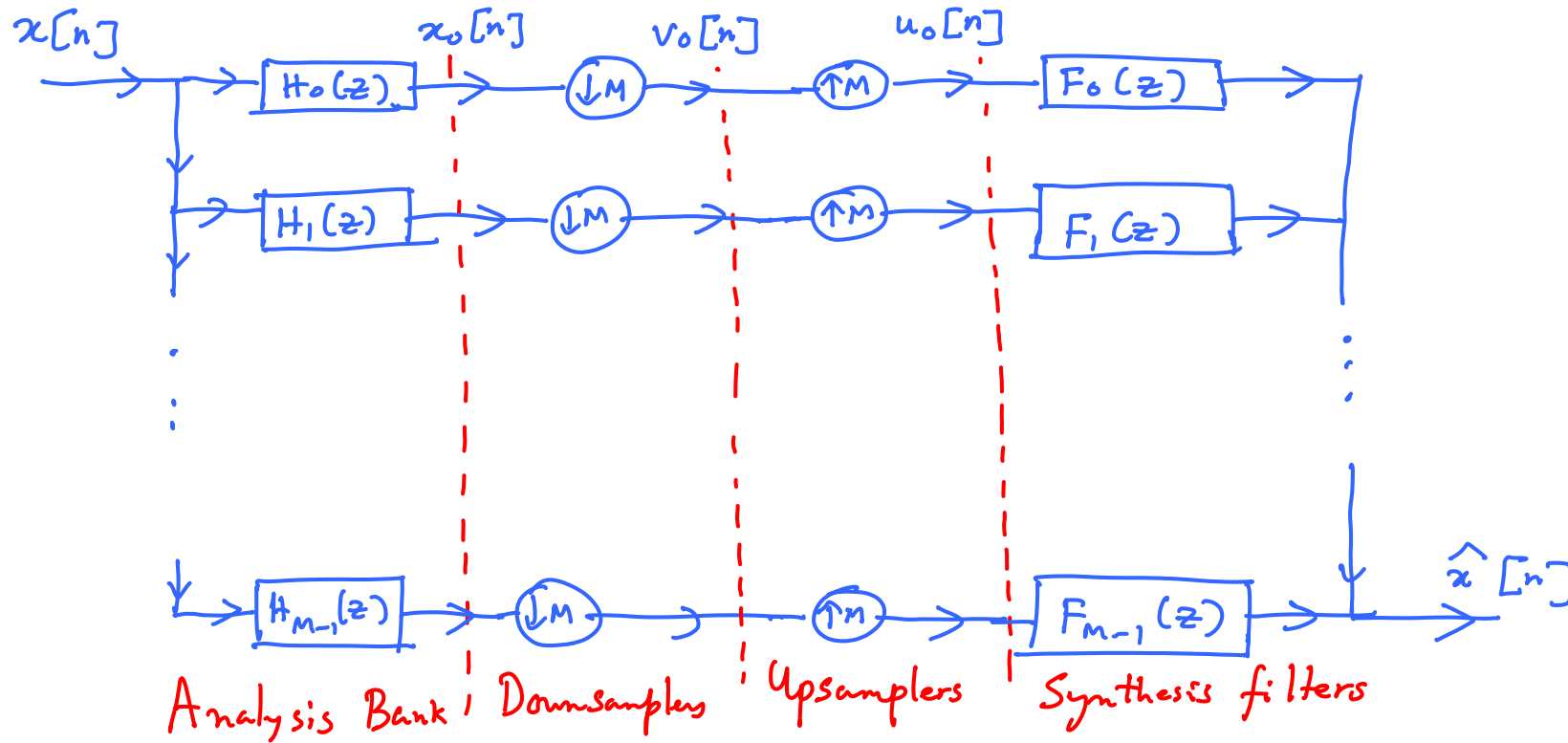
$$u_1[n] + u_0[n-1] = \left\{ \begin{array}{cccccccc} x & 1 & 2 & 3 & 4 & 5 & 6 & 7 \dots \end{array} \right\}$$

NOTE:

We have P.R.
with a delay
of 1 unit
i.e., z^{-1}

M-channel Filter Banks

(GENERALIZATION)



let $\underline{h}(z) = \begin{bmatrix} H_0(z) \\ H_1(z) \\ \vdots \\ H_{M-1}(z) \end{bmatrix}$

Analysis Bank

$\underline{f}(z) = \begin{bmatrix} F_0(z) \\ F_1(z) \\ \vdots \\ F_{M-1}(z) \end{bmatrix}$

transposed synthesis filters

$\underline{e}(z) = \begin{bmatrix} 1 \\ z^{-1} \\ \vdots \\ z^{-(M-1)} \end{bmatrix}$

delay chain needed for poly phase representation

$$X_k(z) = H_k(z) X(z) \quad k = 0, 1, \dots, M-1$$

$$V_k(z) = \frac{1}{M} \sum_{l=0}^{M-1} X(z^{\frac{1}{M}} \omega^l) H_k(z^{\frac{1}{M}} \omega^l) \quad \omega = e^{-j\frac{2\pi}{M}}$$

$$U_k(z) = V_k(z^M) = \frac{1}{M} \sum_{l=0}^{M-1} X(z \omega^l) H_k(z \omega^l)$$

$$\hat{X}(z) = \sum_{k=0}^{M-1} F_k(z) U_k(z) = \frac{1}{M} \sum_{l=0}^{M-1} X(z \omega^l) \sum_{k=0}^{M-1} H_k(z \omega^l) F_k(z)$$

Rewriting in an easier way,

$$\hat{X}(z) = \sum_{l=0}^{M-1} A_l(z) X(z \omega^l) \quad 0 \leq l \leq M-1$$

where $A_l(z) = \frac{1}{M} \sum_{k=0}^{M-1} H_k(z \omega^l) F_k(z)$

With $z = e^{j\omega}$

$$X(e^{j\omega} \omega^l) = X\left(e^{j\left(\omega - \frac{2\pi l}{M}\right)}\right)$$

$X(z \omega^l)$ for $1 \leq l \leq M-1$ are "ALIAS COMPONENTS"

To avoid aliasing $A_l(z) = 0 \quad 1 \leq l \leq M-1$

$$\text{Let } \underline{A}(z) = \begin{bmatrix} A_0(z) \\ A_1(z) \\ \vdots \\ A_{M-1}(z) \end{bmatrix}$$

$$\text{Let } H(z) = \begin{bmatrix} H_0(z) & H_1(z) & \dots & H_{M-1}(z) \\ H_0(z\omega) & H_1(z\omega) & \dots & H_{M-1}(z\omega) \\ \vdots & \vdots & \ddots & \vdots \\ H_0(z\omega^{M-1}) & H_1(z\omega^{M-1}) & \dots & H_{M-1}(z\omega^{M-1}) \end{bmatrix} \begin{array}{l} \text{Alias component} \\ \text{matrix} \\ M \times M \end{array}$$

With aliasing canceled out, the distortion function

$$T(z) = \frac{1}{M} \sum_{k=0}^{M-1} H_k(z) F_k(z) = A_0(z)$$

Now

$$M \begin{bmatrix} A_0(z) \\ \vdots \\ A_{M-1}(z) \end{bmatrix} = \mathbf{H}(z) \underline{f(z)} = \underline{t(z)}$$

But $A_l(z) = 0$ for $1 \leq l \leq M-1$

$$\underline{t(z)} = M \begin{bmatrix} A_0(z) \\ \vdots \\ 0 \end{bmatrix} = M \begin{bmatrix} T(z) \\ 0 \\ \vdots \\ 0 \end{bmatrix}$$

$$\begin{aligned}\hat{X}(z) &= A^T(z) \underline{X}(z) \\ &= \frac{1}{M} \underline{f}^T(z) \underline{A}^T(z) X(z)\end{aligned}$$

where $\underline{X}(z) = \begin{bmatrix} X(z) \\ X(z\omega) \\ \vdots \\ X(z\omega^{(M-1)}) \end{bmatrix}$

Now,

$$\underline{f}(z) = H^{-1}(z) t(z)$$

(Realizable if $H^{-1}(z)$ exists)

For P. R.,

$$\underline{t}(z) = c \begin{bmatrix} z^{-n_0} \\ 0 \\ \dots \\ 0 \end{bmatrix}$$

Difficulties with AC inversion matrix

a) Unless $|H(z)|$ is $\neq 0$ for every z , we are in trouble towards getting $H^{-1}(z)$

b)
$$\underline{f}(z) = \frac{1}{\det(H(z))} \text{adj}(H(z)) \underline{z}$$

← Can give rise to a denominator poly. which may not be just a 'delay' with a 'gain'.

Even if analysis filters are FIR, Synthesis filters can be IIR
⇒ Stability can be a 'problem'!

c) If $\det(H(z))$ has zero on the unit circle i. e., $z = e^{j\omega_0}$
transfer fcn. for unaliased part
then $|T(e^{j\omega_0})| = 0$
 \Rightarrow Severe amplitude distortion around ω_0 !

Singularity of $H(e^{j\omega})$ vs. amplitude distortion

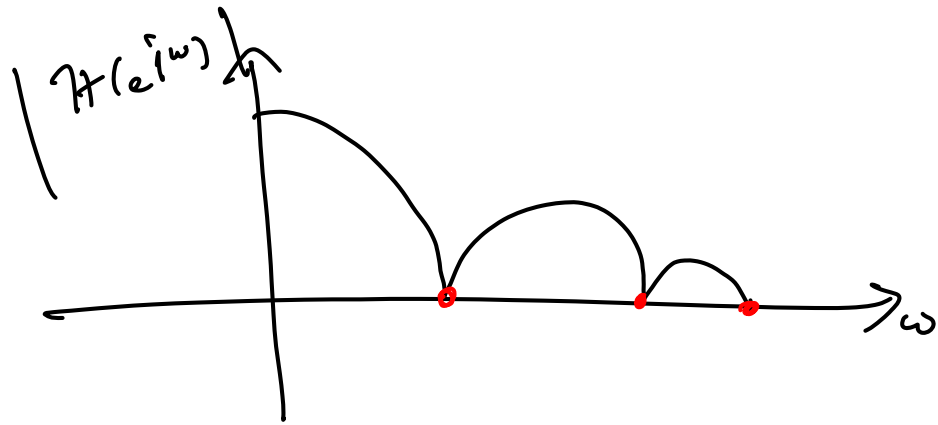
If $T(z)$ has a zero @ $z = e^{j\omega_0}$, then

$$\underline{t}(e^{j\omega_0}) = 0$$

$$\Rightarrow \underline{H}(e^{j\omega_0}) \underline{f}(e^{j\omega_0}) = 0$$

$\underline{H}(e^{j\omega_0})$ is 'singular' unless all synthesis filters

$F_k(z)$ have a zero @ ω_0



Polyphase Representation for M-channel Filter Banks

From our previous discussion, by polyphase representation,

$$H_k(z) = \sum_{l=0}^{M-1} z^{-l} E_{kl}(z^M) \quad \left(\begin{array}{l} \text{Type 1} \\ \text{representation} \end{array} \right)$$

for analysis filters

$$E(z^M)$$

$$\underline{e}(z)$$

We may write

$$\underline{h}(z) \begin{bmatrix} H_0(z) \\ \vdots \\ H_{M-1}(z) \end{bmatrix} = \begin{bmatrix} E_{0,0}(z^M) & E_{0,1}(z^M) & \dots & E_{0,M-1}(z^M) \\ \vdots & \ddots & & \vdots \\ E_{M-1,0}(z^M) & \dots & & E_{M-1,M-1}(z^M) \end{bmatrix} \begin{bmatrix} 1 \\ z^{-1} \\ \vdots \\ z^{-(M-1)} \end{bmatrix}$$

$\underline{h}(z) = E(z^M) \underline{e}(z)$

|||ly, we can do this for the synthesis filters

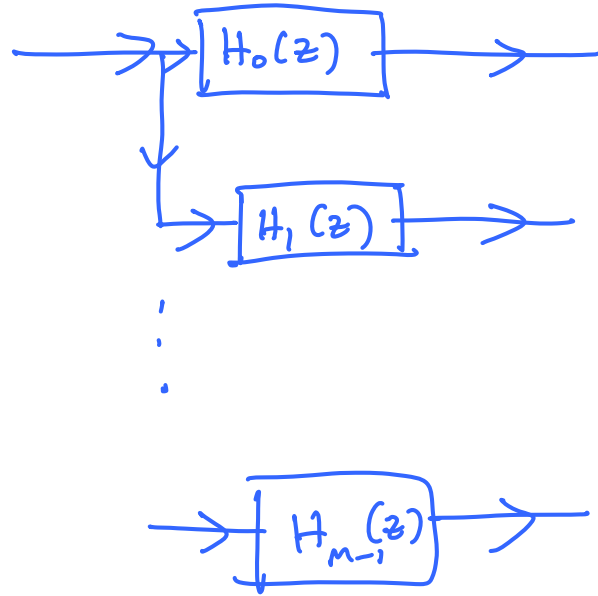
$$F_k(z) = \sum_{l=0}^{M-1} z^{-(M-1-l)} R_{lk}(z^M)$$

Using Type 2 polyphase representation

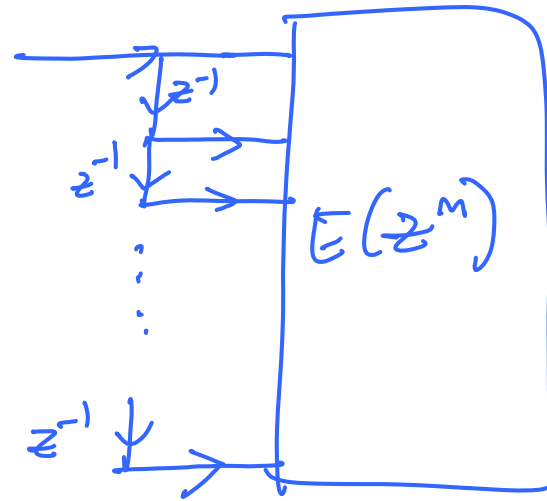
$$\underbrace{[F_0(z) \dots F_{M-1}(z)]}_{\underline{f^T(z)}} = \underbrace{\begin{bmatrix} z^{-(M-1)} & & \\ & \dots & \\ & & 1 \end{bmatrix}}_{z^{-(M-1)} \underline{\tilde{e}(z)}} \underbrace{\begin{bmatrix} R_{0,0}(z^M) & \dots & R_{0,M-1}(z^M) \\ \vdots & \ddots & \vdots \\ R_{M-1,0}(z^M) & & R_{M-1,M-1}(z^M) \end{bmatrix}}_{R(z^M)}$$

$$\underline{f^T(z)} = z^{-(M-1)} \underline{\tilde{e}(z)} R(z^M)$$

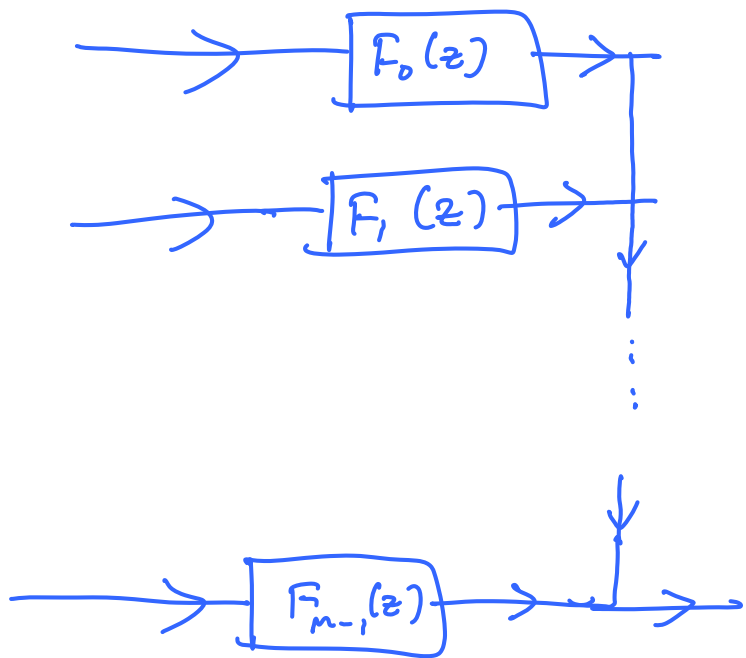
$$\underline{\tilde{e}(z)} = \underline{e(z)}^T$$



|||

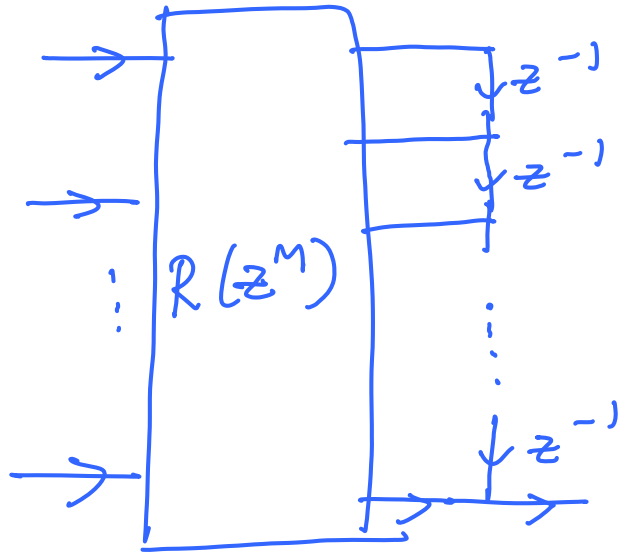


Analysis Bank

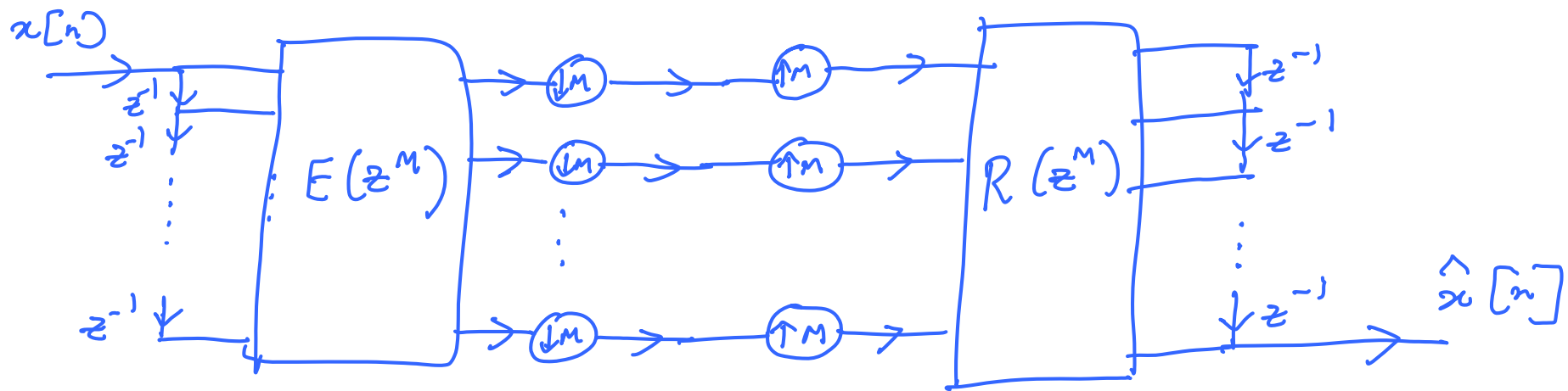


Synthesis Bank

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(Type 2 poly phase)

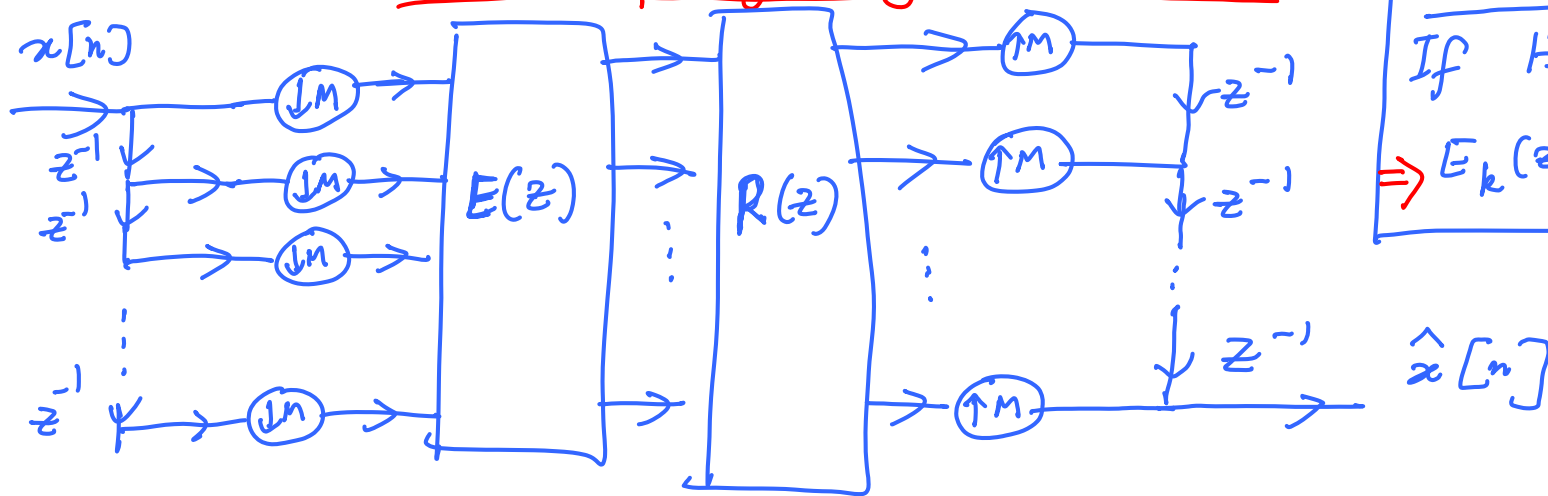


Architecture - I

Trick:

Apply Noble Identities to simplify Arch. I further towards analysis on P. R. properties

A lot of Symmetry in Arch. II



Architecture - II

Aside:
 If $H_k(z)$ is causal
 $\Rightarrow E_k(z)$ is causal

$P(z) = E(z) R(z)$
 Goal: Choose $R(z)$ to meet the design specs (alias free, P.R.)
 If $P(z) = I$, we are left with a delay filter bank

From our previous discussion on polyphase decomposition, we saw

$$P(z) = R(z)E(z)$$

$$\text{If } P(z) = I \implies R(z) = E^{-1}(z)$$

Theorem: (TASSP 1987)

(Exercise: Go through the proof)

A necessary and sufficient condition for the P.R. property is $P(z)$ must take one of the following forms i.e.,

$$P(z) = d \begin{bmatrix} z^{-k} & 0 \\ 0 & z^{-k} \end{bmatrix} \text{ or } P(z) = d \begin{bmatrix} 0 & z^{-k} \\ z^{-k-1} & 0 \end{bmatrix}$$

$$E(z) = \begin{bmatrix} E_0(z) & E_1(z) \\ E_0(z) & -E_1(z) \end{bmatrix} \quad R(z) = \begin{bmatrix} E_1(z) & E_1(z) \\ E_0(z) & -E_0(z) \end{bmatrix}$$

$$\begin{aligned} R(z)E(z) &= \begin{bmatrix} 2E_0(z)E_1(z) & 0 \\ 0 & 2E_0(z)E_1(z) \end{bmatrix} \\ &= 2E_0(z)E_1(z) \underbrace{\begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}} \end{aligned}$$

Now, a system is PR iff $E_0(z) E_1(z)$ is a pure delay

If $H_0(z)$ is constrained to be a FIR, it is possible

iff $E_0(z)$ and $E_1(z)$ are pure delays

$\Rightarrow H_0(z)$ must be of the form

$$H_0(z) = c_0 z^{-2n_0} + c_1 z^{-(2n_1+1)}$$

If we need a FIR, we may have to give up on

$$H_1(z) = H_0(-z)$$

Idea :

For a general PR, we let $R(z) = d z^{-k} E^{-1}(z)$

a) If $E(z)$ is min ϕ , $R(z)$ hence $\{F_k(z)\}$ will
be LIR but 'stable'

b) If somehow $\det(E(z))$ lands as a 'delay' we
can hopefully construct FIR PR QMF banks

$\det(E(z)) = z^{-n_0} \Rightarrow$ Family of lossless matrices
This is however not a necessary condition for PR.

Example :

Suppose

$$H(z) = \begin{bmatrix} 1+z^{-1} & 1-z^{-1} \\ 1-z^{-1} & 1+z^{-1} \end{bmatrix}$$

$$H(z) \overline{H(z)} = c I \quad (\text{lossless})$$

$$H^{-1}(z) = \frac{1}{4} \begin{bmatrix} 1+z & 1-z \\ 1-z & 1+z \end{bmatrix}$$

Suppose $R(z) = c z^{-k} E^{-1}(z)$. Consider $E(z) = H(z)$

(I)

We plug in $k=1, c=4$

$$R(z) = \begin{bmatrix} 1+z^{-1} & z^{-1}-1 \\ z^{-1}-1 & 1+z^{-1} \end{bmatrix}$$

$$E(z) = H(z)$$

$$\begin{aligned} H_0(z) &= E_{00}(z^2) + z^{-1} E_{01}(z^2) \\ &= 1 + z^{-2} + z^{-1} (1 - z^{-2}) \\ &= 1 + z^{-1} + z^{-2} - z^{-3} \end{aligned}$$

$$\begin{aligned}
 H_1(z) &= E_{10}(z^2) + z^{-1} E_{11}(z^2) \\
 &= 1 - z^{-2} + z^{-1} (1 + z^{-2}) \\
 &= 1 + z^{-1} - z^{-2} + z^{-3}
 \end{aligned}$$

} Analysis filters
 H_0, H_1 are FIR

Similarly for the synthesis bank,

$$\begin{aligned}
 F_0(z) &= z^{-1} R_{00}(z^2) + R_{10}(z^2) \\
 F_1(z) &= z^{-1} R_{01}(z^2) + R_{11}(z^2) \\
 F_0(z) &= z^{-1} (1 + z^{-2}) + z^{-2} - 1 = -1 + z^{-1} + z^{-2} + z^{-3} \\
 F_1(z) &= 1 - z^{-1} + z^{-2} + z^{-3}
 \end{aligned}$$

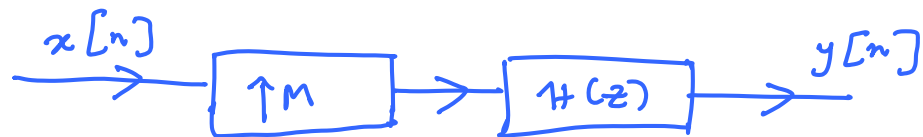
} Synthesis filters are FIR

Special Filters and Properties

Mth band / Nyquist M filters

From polyphase decomposition,

$$H(z) = c + z^{-1} E_1(z^M) + z^{-2} E_2(z^M) + \dots + z^{-(M-1)} E_{M-1}(z^M)$$



$$\begin{aligned} Y(z) &= X(z^M) H(z) \\ &= \underbrace{c X(z^M)} + \sum_{l=1}^{M-1} z^{-l} E_l(z^M) X(z^M) \end{aligned}$$

$$y(Mn) = c x(n) \quad \text{by considering just the 1st poly phase component!}$$

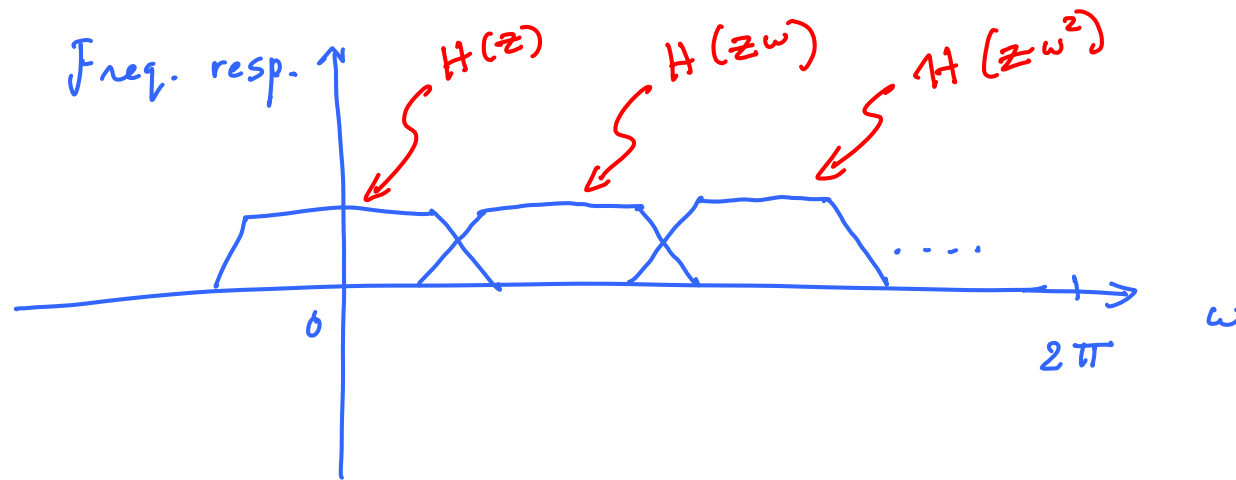
*
 Suppose $h(Mn) = \begin{cases} c & n = 0 \\ 0 & \text{else} \end{cases}$

From the representation of $H(z)$ in the polyphase form,

$$\sum_{k=0}^{M-1} H(z\omega^k) = c + z^{-1} E_1(z^M) + \dots + z^{-(M-1)} E_{M-1}(z^M) \\
+ c + z^{-1} \omega^{-1} E_1(z^M \omega^M) + \dots + z^{-(M-1)} \omega^{-(M-1)} E_{M-1}(z^M \omega^M) \\
\vdots \\
+ c + z^{-1} \omega^{-(M-1)} E_1(z^M \omega^{(M-1)M}) + \dots + z^{-(M-1)} \omega^{-(M-1)(M-1)} E_{M-1}(z^M \omega^{(M-1)M})$$

$$cM + z^{-1} \underbrace{[1 + \omega^{-1} + \dots + \omega^{-(M-1)}]}_0 E_1(\cdot) + \dots$$

If $c = \frac{1}{M} \Rightarrow \sum_{k=0}^{M-1} H(z\omega^k) = 1$



Ponder ; Why are these called 'Nyquist' M filters?
 What is the cross over frequency for each pair of adjacent freq. responses?

Half band filters

This is a special case of the Nyquist $M = 2$ filters.

$$H(z) = c + z^{-1} E_1(z^2)$$

$$h(2n) = \begin{cases} c & n = 0 \\ 0 & \text{else} \end{cases}$$

Examples:

$$H(z) = \begin{cases} 1 + z^{-3} \\ z + 1 + z^{-1} \\ 1 + z^{-1} + z^{-3} \end{cases}$$

$$E_1(z) = z^{-1}$$

$$E_1(z) = 1 + z \quad (\text{anti causal})$$

$$E_1(z) = 1 + z^{-1} \quad (\text{causal})$$

Filters have linear phase, but could be causal/anti causal!

VERIFICATION

$$H(-z) = H(e^{j(\pi+\omega)})$$

$$H(e^{j\omega}) + H(e^{j(\pi+\omega)}) = 1$$

symmetric around $\pi/2$!

NOTES

- 1) One can design good half band filters using mirror symmetric properties.
- 2) The generalization to Nyquist M_r filter design can be carried out through optimization techniques.

System Level Properties

A. Strictly Complementary Functions (SC)

$[H_0(z) \ H_1(z) \ \dots \ H_{M-1}(z)]$ are

responses add to delay.

$$\sum_{k=0}^{M-1} H_k(z) = c z^{-n_0}$$

S.C. if their

$$c \neq 0$$

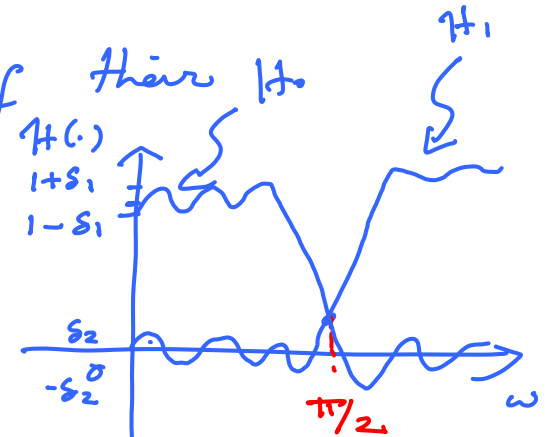


Fig: Case $M=2$
 $c=1, n_0=N/2$

For $M=2$ case, with $c=1$ and $n_0=N/2$,

$$H_0(e^{j\omega}) = e^{-j\omega N/2} H_R(\omega)$$

$$\Rightarrow \begin{aligned} H_1(z) &= z^{-N/2} - H_0(z) \\ H_1(e^{j\omega}) &= e^{-j\omega N/2} (1 - H_R(\omega)) \end{aligned}$$

B. Power Complementary

$$\sum_{k=0}^{M-1} |H_k(e^{j\omega})|^2 = c \quad \forall \omega$$

$$\Rightarrow \sum_{k=0}^{M-1} H_k(e^{j\omega}) \tilde{H}_k(e^{j\omega}) = c$$

From P. R. perspective, one can choose $F_k(z) = \tilde{H}_k(z)$
 To ensure causality, one can impose delay constraints into $\tilde{H}_k(z)$
 so that the o/p is delayed

For $M=2, c=1$ PC

$$|H_1(e^{j\omega})|^2 = 1 - |H_0(e^{j\omega})|^2$$

$\therefore H_1(e^{j\omega})$ is a spectral factor of $1 - |H_0(e^{j\omega})|^2$

C. All Pass Complementary

$$\sum_{k=0}^{M-1} H_k(z) = A(z)$$

where $A(z)$ is an all pass filter

S.C \Rightarrow A.P.C / but not "otherwise"

Re construction is free from 'amplitude distortion'

D. Doubly Complementary

$\{ H_k(z) \}_{k=0}^{M-1}$ satisfying both P.C. & A.P.C.
are doubly complementary